

A norm-based point of view for fault diagnosis: Application to aerospace missions.

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Outline of the talk

- ➊ Motivations for "norm-based" theory
- ➋ Objectives and problem setting: the LTI case
- ➌ The solution
- ➍ The μ_g -post-analysis procedure
- ➎ Aerospace examples
- ➏ Concluding remarks (extension to LPV problems)

Preliminaries

matching the keywords "fault detection"

- *The SciVerse - ScienceDirect database*
→ returns more than 40200 records
 - *The IEEE database:*
→ returns more than 12970 records
 - *The AIAA database:*
→ returns more than 200 records

- FDI: a very active research topic in both academic and aerospace industrial institutions
 - Not an exhaustive list of existing methods (hardware and model-based, FDI / DX communities)
 - Model-based methods applied (with potential applications) to aerospace problems

Motivations

- Two main approaches
 - Fault estimation $\Rightarrow \min$ optimization problem e.g. following the Kalman's "*Prediction - Correction cycle*" or the "*Unknown Input estimation technique*".
 - Residual generation problem $\Rightarrow \min / \max$ optimization problem

Linear approaches

$$r(s) = H_y(s)y(s) + H_u(s)u(s) \quad r(s) = G_d(\theta, s)d(s) + G_f(\theta, s)f(s)$$

- Two main solutions

Decoupling approaches

$$G_d(\theta, s)d(s) = 0$$

$G_f(\theta, s)f(s) \Rightarrow$ fault detectability.

- "perfect" robustness level
 - $\perp \text{span}\{d\}$ and $\parallel \text{span}\{f\}$ may not exist
 - Isolation problem: Rank conditions (often) not satisfied

An alternative framework: "Approximated" decoupling

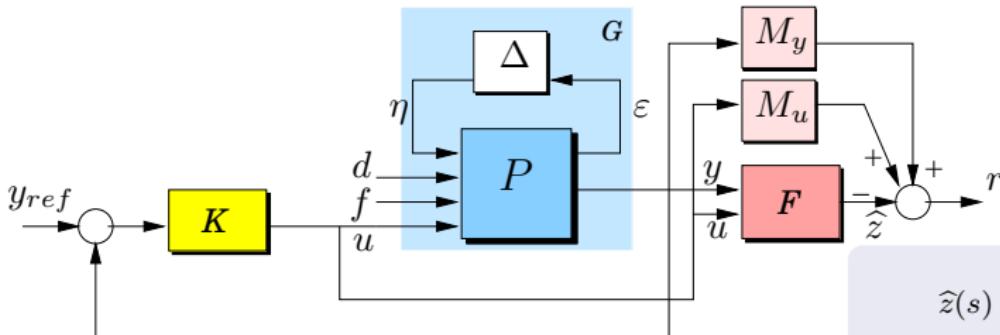
$\Rightarrow \min h_1(T_{rd}) / \max h_2(T_{rf})$ with poles assignment

$$h_1 \in \{H_2, H_{2g}, H_\infty\} \quad h_2 \in \{H_-, H(0)\}$$

- ① H_∞ specifications: to enforce robustness to model uncertainty (e.g. external disturbances, parametric uncertainties and neglected dynamics).
- ② $H(0)/H_-$ specifications: for fault sensitivity requirements over specified frequency ranges.
- ③ H_2 objectives: to take into account the stochastic nature of disturbances.
- ④ $H_{2g} +$ poles assignment: to tune the transient response and to enforce some minimum decay rate of the residuals.

Remark: H_2 not useful for fault sensitivity specifications (Zhou, 2009).

The proposed solution



$$\hat{z}(s) = F(s) \begin{pmatrix} y(s) \\ u(s) \end{pmatrix}$$

$$r(t) = \textcolor{red}{M_y}y(t) + \textcolor{red}{M_u}u(t) - \widehat{z}(t)$$

- The LFR paradigm: nonlinear parametric uncertainties, neglected dynamics, flexible modes (Beck et al., 1996; Cockburn and Morton, 1997; Varga et al., 1998; Beck and Doyle, 1999; Hecker et al., 2005)

$$\begin{aligned} y &= \mathcal{F}_u(P, \Delta) \begin{pmatrix} d^T & f^T & u^T \end{pmatrix}^T, \Delta \in \underline{\Delta} : \|\Delta\|_\infty \leq 1, \\ \underline{\Delta} &= \left\{ \text{block diag}(\delta_1^r I_{k_1}, \dots, \delta_{m_r}^r I_{k_{m_r}}, \delta_1^c I_{k_{m_r+1}}, \dots, \delta_{m_c}^c I_{k_{m_r+m_c}}, \right. \\ &\quad \left. \Delta_1^C, \dots, \Delta_{m_C}^C), \delta_i^r \in \mathbb{R}, \delta_i^c \in \mathbb{C}, \Delta_i^C \in \mathbb{C} \right\} \end{aligned}$$

- Takes into account the controller actions
 - M_y, M_u : "merge optimally" input/output signals

Problem formulation

Let f be detectable faults (Massoumnia et al., 1989; Chung and Speyer, 1998; Zad and Massoumnia, 1999; Saberi et al., 2000) and

assume $\sup_{\omega} \mu_{\Delta} \mathcal{F}_l((P, K)(j\omega)) < 1$. The goal is to find $M_y \in \mathbb{R}^{q_r \times m}$, $M_u \in \mathbb{R}^{q_r \times p}$ (constant), $A_F \in \mathbb{R}^{n_F \times n_F}$, $B_F \in \mathbb{R}^{n_F \times (p+m)}$, $C_F \in \mathbb{R}^{q_r \times n_F}$ and $D_F \in \mathbb{R}^{q_r \times (p+m)}$ so that r solves the optimization problem:

$$\textcircled{1} \quad \min_{M_y, M_u, F} \gamma_1 \quad \begin{aligned} & \forall \Delta \in \underline{\Delta} : \|\Delta\|_\infty \leq 1 \\ & \text{s.t. } \|T_{rd}\|_\infty < \gamma_1 \end{aligned} \quad (\text{Robustness})$$

$$② \max_{M_y, M_u, F} \gamma_2 \quad \begin{aligned} & \forall \Delta \in \Delta : ||\Delta||_\infty \leq 1 \\ & \text{s.t. } ||T_{rf}||_- > \gamma_2 \quad \forall \omega \in \Omega \end{aligned} \quad (\text{Fault sensitivity})$$

③ $\lambda_i \{A_F\} \in \mathcal{D}$ with \mathcal{D} left-half plane (Poles assignment)

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$$M_y \in \mathbb{R}^{q_r \times m}, M_u \in \mathbb{R}^{q_r \times p} \text{ (constant)}, A_F \in \mathbb{R}^{n_F \times n_F},$$

$B_F \in \mathbb{R}^{n_F \times (p+m)}$, $C_F \in \mathbb{R}^{q_r \times n_F}$ and $D_F \in \mathbb{R}^{q_r \times (p+m)}$ so that r solves

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③ $\lambda_i \{A_F\} \in \mathcal{D}$ with \mathcal{D} left-half plane (Poles assignment)

Remark: The smallest gain (Chen & Patton, 1999; Rank & Niemann, 1999; Henry, 2005): $\|P\|_- = \inf_{\omega \in \Omega} \underline{\sigma}(P(j\omega))$, $\Omega = [\omega_1 ; \omega_2]$ → differs from (Liu et al., 2005; Wei and Verhaegen, 2008), i.e. defined on a infinite frequency horizon

The LMI solution derived in 3 steps

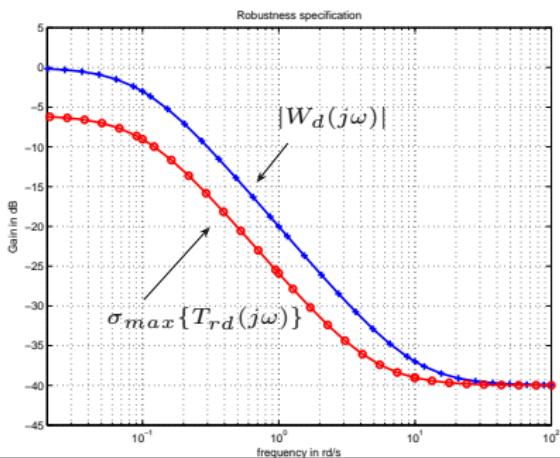
- ① Specify the robustness and sensitivity objectives + poles assignment → "shaping filters" + LMI Regions.
- ② The quasi-standard form → algebra manipulations on LFRs.
- ③ Use of the bounded real (Boyd, 1994) and the projection lemmas (Gahinet & Apkarian, 1994) using an appropriate basis, to derive a SDP formulation.

Robustness objectives (shaping filter W_d)

Let $W_d : ||W_d||_\infty \leq \gamma_1$ be the shaping filters associated to T_{rd} . Then the robustness requirements are satisfied iff

$$\exists M_y, M_y, F : \|T_{rd}W_d^{-1}\|_\infty < 1 \quad \square$$

- Illustrative example: noise measurement rejection (to understand).
 - Objective: attenuation of $40dB$ (**at least**) for $\omega \in [10rd/s; +\infty[$



$$W_d(s) = 10^{-2} \frac{s+10}{s+0.1}$$

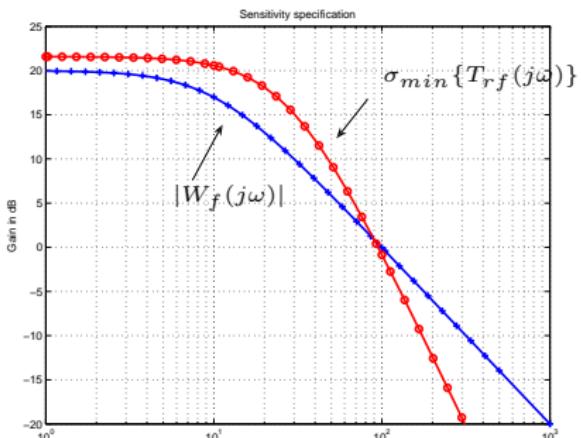
$$\sigma_{max}\{Tr_d(j\omega)\} < |W_d(j\omega)| \\ \Leftrightarrow \|Tr_d W_d^{-1}\|_\infty < 1$$

Fault sensitivity objectives (shaping filter W_f)

Let W_F be an invertible LTI transfer matrix defined such that $\|W_f\|_- = \gamma_2/\lambda \|W_F\|_-$ and $\|W_F\|_- > \lambda$ where $\lambda = 1 + \gamma_2$. Define the (fictitious) signal \tilde{r} such that $\tilde{r} = r - W_F f$. Then fault sensitivity objective is satisfied if (**sufficient condition**)

$$\exists M_y, M_u, F : \|T_{\tilde{r}f}\|_\infty < 1 \quad \square$$

Proof: (Henry, 2005)

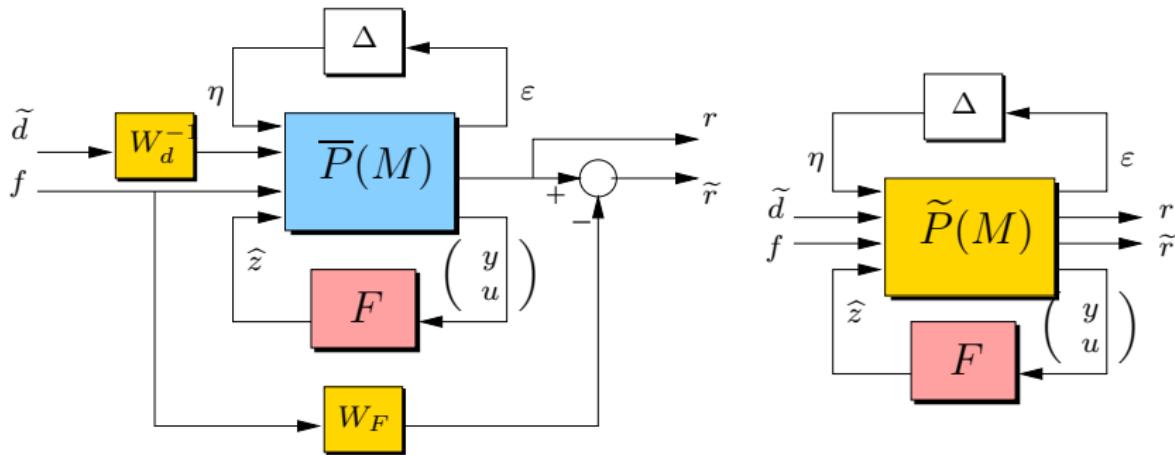


Illustrative example
 \Rightarrow amplification of 20dB (at least) for $\omega \in]0; 100] \text{rd/s}$

$$\sigma_{min}\{T_{rf}(j\omega)\} > |W_f(j\omega)|$$

$$\Leftrightarrow \|T_{rf}W_f^{-1}\|_- > 1 \forall \omega \in \Omega$$

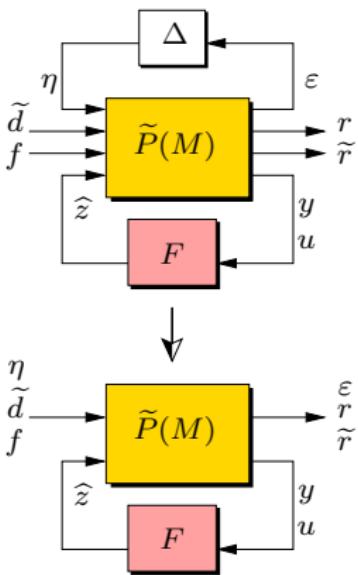
The quasi-standard problem



Let $M = [M_y \ M_u] \in \mathbb{R}^{q_r \times (m+p)}$. Including W_d^{-1} and W_F into $\overline{P}(M)$. Then, after some LFR manipulations, it follows that $(M_y, M_u, F(s))$ solves the problem iff:

$$\left\| \mathcal{F}_u \left(\mathcal{F}_l \left(\widetilde{P}(M), F \right), \Delta \right) \right\|_{\infty} < 1$$

The quasi-standard problem



Small gain theorem (Zames,64)

$$\left\| \mathcal{F}_u \left(\mathcal{F}_l \left(\tilde{P}(M), F \right), \Delta \right) \right\|_{\infty} < 1 \quad \forall \Delta \in \underline{\Delta} : \|\Delta\|_{\infty} \leq 1$$

$$\text{if } \left\| \mathcal{F}_l \left(\tilde{P}(M), F \right) \right\|_{\infty} < 1 \quad \square$$

$$\tilde{P}(M) = \left[\begin{array}{c|cc} \tilde{A} & \tilde{B}_1 & \tilde{B}_2 \\ \hline \tilde{C}_1 & \tilde{D}_{11} & \tilde{D}_{12} \\ \tilde{C}_2 & \tilde{D}_{21} & \tilde{D}_{22} \end{array} \right]$$

$$\tilde{B}_2 = 0, \tilde{D}_{22} = 0, \tilde{D}_{12} = \begin{pmatrix} 0 \\ -I_{2 \times q_r} \end{pmatrix}$$

Remark: Not a standard H_∞ problem since $\tilde{P}(M) \quad M = (M_y \ M_u)$
 \Rightarrow "hinfsyn" / "hinflmi" not applicable

The SDP formulation

Proposition (Henry, 2005)

Let $W = (\tilde{C}_2 \quad \tilde{D}_{21})^\perp$. Then $(M_y, M_u, F(s))$ solve the SDP problem
iff $\exists M_y \in \mathbb{R}^{q_r \times m}$, $M_u \in \mathbb{R}^{q_r \times p}$ and matrices $R = R^T > 0$ and
 $S = S^T > 0$ that solve the following SDP problem:

$$\begin{aligned} & \min \gamma \\ s.t. & \left(\begin{array}{ccc} \tilde{A}R + R\tilde{A}^T & R\hat{C}_1^T & \tilde{B}_1 \\ \hat{C}_1R & -\gamma I_w & \hat{D}_{11} \\ \tilde{B}_1^T & \hat{D}_{11}^T & -\gamma I_{v+q_{\tilde{d}}+q_f} \end{array} \right) < 0 \\ & \left(\begin{array}{c|c} W & 0 \\ \hline 0 & I \end{array} \right)^T \left(\begin{array}{cc|c} \tilde{A}^T S + S\tilde{A} & S\tilde{B}_1 & \tilde{C}_1^T(M) \\ \tilde{B}_1^T S & -\gamma I_{v+q_{\tilde{d}}+q_f} & \tilde{D}_{11}^T(M) \\ \hline \tilde{C}_1(M) & \tilde{D}_{11}(M) & -\gamma I_{w+2q_r} \end{array} \right) \left(\begin{array}{c|c} W & 0 \\ \hline 0 & I \end{array} \right) < 0 \\ & \left(\begin{array}{cc} R & I \\ I & S \end{array} \right) \geq 0 \end{aligned}$$

$$\widehat{C}_1 = \begin{pmatrix} C_1 & D_{1d}C_{wd} & 0_{w \times n_{wF}} \end{pmatrix}, \quad \widehat{D}_{11} = \begin{pmatrix} D_{11} & D_{1d}D_{wd} & D_{1f} \end{pmatrix}$$

Proof Bounded real lemma + projection lemma in a judiciously chosen basis.

The numerical procedure

- ➊ Solve the SDP problem (SDPT3, CSDP, DSDP5 ...etc...) \Rightarrow the optimal solution (γ, R, S, M_y, M_u)
- ➋ Compute M, N so that $MN^T = I - RS \rightarrow$ SVD
- ➌ Compute the Lyapunov matrix X_{cl} (those involves in the bounded real lemma)

$$\begin{pmatrix} R & I \\ M^T & 0 \end{pmatrix} = \begin{pmatrix} I & S \\ 0 & N^T \end{pmatrix}$$

- ➍ Find A_F, B_F, C_F, D_F so that

$$\begin{pmatrix} A_{cl}^T X_{cl} + X_{cl} A_{cl} & X_{cl} B_{cl} & C_{cl}^T \\ B_{cl}^T X_{cl} & -\gamma I_{v+q_d+q_f} & D_{cl}^T \\ C_{cl} & D_{cl} & -\gamma I_{w+2q_r} \end{pmatrix} < 0$$

\rightarrow using a SDP solver (SDPT3, CSDP, DSDP5 ...etc...)
 \rightarrow using some linear algebra (Gahinet et Apkarian, 94)

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→ using a SDP solver (SDPT3, CSDP, DSDP5 ...etc...)

→ using some linear algebra (Gahinet et Apkarian, 94)

Computational issues

- Since the procedure involves $MN^T = I - RS \Rightarrow I - RS$ has to be well conditioned .
- Unfortunately, $I - RS$ will be nearly singular if the constraint $\begin{pmatrix} R & I \\ I & S \end{pmatrix} \geq 0$ is saturated at the optimum.

Solution

Maximize the minimal eigenvalue of RS to push all eigenvalues away from "1", i.e.

$$\begin{aligned} \min \gamma + \varepsilon \rho &\quad s.t \\ \begin{pmatrix} R & \rho I \\ \rho I & S \end{pmatrix} &\geq 0 \quad \text{with } \varepsilon < 0 \end{aligned}$$

Computational issues

Since we optimize M_y , M_u and F simultaneously

⇒ no unique solution for M_y , M_u and D_F , i.e. the static part of F
→ $r(t)$ includes the subtraction of these two parts.

Solution

- ① Add constraints on $M = [M_y \ M_u]$ to the LMIs
- ② and/or add an optimization objective on some functional of M

$$\sum_j M_{ij} = 1, \quad \forall i$$

Remark: Following my own experience: $D_F = 0$ (Henry, 2005; Henry, 2006; Falcoz et al. 2008; Henry, 2008; Falcoz et al., 2010).

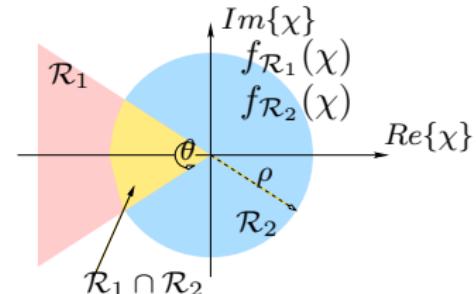
Robust poles assignment

Definition(Chilali et Gahinet, 1996):

\mathcal{R} is called a LMI region if $\exists L = L^T, Q = Q^T$:

$$\mathcal{R} = \{\chi \in \mathbb{C} : f_{\mathcal{R}}(\chi) = L + \chi Q + \chi^* Q^T < 0\}$$

$f_{\mathcal{R}}(\chi)$ = characteristic function of \mathcal{R} .



Proposition (Henry, 2005b)

$\lambda_i \{A_F\} \in \mathcal{R} = \mathcal{R}_1 \cap \dots \cap \mathcal{R}_N, \forall i, \forall \Delta \in \underline{\Delta} : \|\Delta\|_\infty \leq 1$ if (**sufficient condition**) $\exists N \ X_i = X_i^T > 0$ t.q.

$$\begin{pmatrix} \mathcal{Q}_{\mathcal{R}_i}(A_{\mathcal{R}}, X_i) & Q_{1i}^T \otimes X_i B_{\mathcal{R}} & Q_{2i}^T \otimes C_{\mathcal{R}}^T \\ Q_{1i} \otimes B_{\mathcal{R}}^T X_i & -I & I \otimes D_{\mathcal{R}}^T \\ Q_{2i} \otimes C_{\mathcal{R}} & I \otimes D_{\mathcal{R}} & -I \end{pmatrix} < 0 \quad i = 1, \dots, N$$

$$\begin{aligned} \rightarrow \mathcal{Q}_{\mathcal{R}_i}(A_{\mathcal{R}}, X_i) &= L_i \otimes X_i + Q_i \otimes X_i A_{\mathcal{R}} + Q_i^T \otimes A_{\mathcal{R}}^T X_i \\ \rightarrow A_{\mathcal{R}}, B_{\mathcal{R}}, C_{\mathcal{R}}, D_{\mathcal{R}} : \text{transfer } (\eta^T \tilde{z}^T)^T &\rightarrow (\varepsilon^T y^T u^T)^T \end{aligned}$$

□

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H_{2g} specifications

Goal: Find $(M_y, M_u, F(s))$ so that.

$$|r(t)|_{||d||_2=1} < \gamma_3 \quad \forall t \Leftrightarrow ||T_{rd}||_{2g} < \gamma_3$$

Proposition (Henry, 2005b)

Given a fictitious signal $r_g \in \mathbb{R}^{q_r}$ so that $r_g = W_g r$, $W_g \in \mathbb{R}^{q_r \times q_r}$, $\|W_g\| = 1/\gamma_3$ and $(A_g, B_g, C_g, D_g) \Rightarrow (d^T \tilde{z}^T)^T \rightarrow (r^T y^T u^T)^T$. Then $\|T_{rd}\|_{2g} < \gamma_3$ if (**necessary** condition) $\exists X_g = X_g^T > 0$ and $\alpha < 1$ so that:

$$\begin{aligned} & \min \alpha \\ \text{s.t. } & \begin{pmatrix} A_g^T X_g + X_g A_g & X_g B_g \\ B_g^T X_g & -I \end{pmatrix} < 0, \quad \begin{pmatrix} X_g & C_g^T \\ C_g & \alpha I \end{pmatrix} > 0 \\ & D_g = 0 \end{aligned}$$

Proof: Based on some results in (Scherer et al, 1997)



Computational procedure

Join all LMIs into a single optimization problem, i.e. find A_F, B_F, C_F, D_F so that:

- H_∞/H_- :
$$\begin{pmatrix} A_{cl}^T X_{cl} + X_{cl} A_{cl} & X_{cl} B_{cl} & C_{cl}^T \\ B_{cl}^T X_{cl} & -\gamma I_{v+q_d+q_f} & D_{cl}^T \\ C_{cl} & D_{cl} & -\gamma I_{w+2q_r} \end{pmatrix} < 0$$
- Robust poles assignment:

$$\begin{pmatrix} \mathcal{Q}_{\mathcal{R}_i}(A_{\mathcal{R}}, X_i) & Q_{1i}^T \otimes X_i B_{\mathcal{R}} & Q_{2i}^T \otimes C_{\mathcal{R}}^T \\ Q_{1i} \otimes B_{\mathcal{R}}^T X_i & -I & I \otimes D_{\mathcal{R}}^T \\ Q_{2i} \otimes C_{\mathcal{R}} & I \otimes D_{\mathcal{R}} & -I \end{pmatrix} < 0 \quad i = 1, \dots, N$$
- H_{2g} specifications:

$$\begin{pmatrix} A_g^T X_g + X_g A_g & X_g B_g \\ B_g^T X_g & -I \end{pmatrix} < 0, \quad \begin{pmatrix} X_g & C_g^T \\ C_g & \alpha I \end{pmatrix} > 0 \quad D_g = 0$$

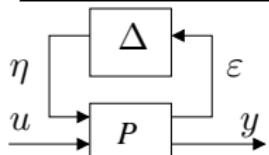
For convexity reasons: $X_{cl} = X_i = X_g$
 \Rightarrow conservative solutions.

An illustrative example

$$\begin{cases} \dot{x} = A(k)x + E_1 d + K_1 f \\ y = Cx \end{cases}, A(k) = \begin{pmatrix} 0 & 1 \\ -k/m & -\zeta/m \end{pmatrix}, C = I_2$$

$$m = 10, \quad \zeta = 10, \quad 8 < k < 12, \quad E_1 = (1 \ 1)^T, \quad K_1 = (1 \ 1)^T$$

- Step 1: The LFR formulation:

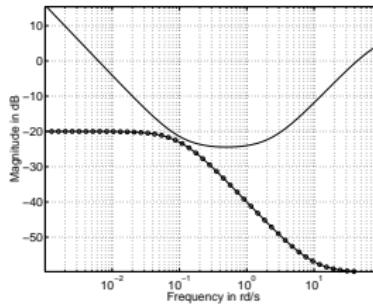


$$y = \mathcal{F}_u(P, \Delta)$$

$$\Delta = \delta_k, \delta_k \in \mathbb{R}, |\delta_k| \leq 1$$

$$k = k_0 + w_k \delta_k, \quad k_0 = 10, \quad w_k = 2.$$

- Step 2: The shaping filters:
 - f in low frequencies
 - d in a limited frequency range



- Step 3: Solve the SDP problem and compute $F(s)$:

Probleme de Synthese de F sur les dimensions:

--> Nb d: 1 / Nb f: 1 / Nb u:1/ Nb y: 1 / Nb r: 1

+ Probleme d'optimization LMI:

ID	Constraint	Type	Tag
1	Numeric value	Matrix inequality 8x8	LMI n1
2	Numeric value	Matrix inequality 8x8	LMI n2
3	Numeric value	Matrix inequality 12x12	LMI RS

+ Minimisation de gamma

+ Solver chosen : **sdpt3-3.02**

+ Processing objective h(x)

+ Processing F(x)

+ Calling SDPT3

***** Infeasible path-following algorithms *****

version	predcorr	gam	expon	scale	data		
NT	1	0.000	1	0			
it	pstep	dstep	p infeas	d infeas	gap	obj	cputime
0	0.000	0.000	9.7e+05	1.0e+01	2.7e+06	-1.470782e-06	
1	0.002	0.033	9.7e+05	9.7e+00	2.7e+06	-2.005763e+02	0.3
2	0.041	0.061	9.3e+05	9.1e+00	2.7e+06	-1.188450e+03	0.3
3	0.174	0.782	7.7e+05	2.0e+00	1.8e+06	-8.102019e+03	0.3
4	0.694	0.844	2.4e+05	3.1e-01	6.7e+05	-1.143302e+04	0.3
5	0.746	0.623	6.0e+04	1.2e-01	2.3e+05	-1.089181e+04	0.3
6	0.878	0.896	7.3e+03	1.2e-02	3.4e+04	-6.294910e+03	0.3
7	0.626	0.800	2.7e+03	2.4e-03	1.6e+04	-3.533212e+03	0.4
8	0.402	1.000	1.6e+03	1.3e-14	1.1e+04	-1.555054e+03	0.4
9	0.850	0.926	2.4e+02	5.2e-15	1.9e+03	-6.850118e+02	0.4

Motivations ooo	The solution ooooooooooooooo●			μ_g	Analysis ooo	Aerospace examples oooooooooooo		Conclusion ooooo
19	0.798	0.565	1.4e-04	8.2e-13	8.5e-01	-9.484335e-01	0.5	
20	0.678	1.000	4.5e-05	9.2e-13	5.5e-01	-9.811465e-01	0.6	
21	0.966	0.955	1.5e-06	8.2e-13	2.5e-02	-9.857646e-01	0.6	
22	0.907	0.967	1.4e-07	2.5e-12	2.4e-03	-9.854703e-01	0.6	
23	0.935	1.000	1.1e-08	1.1e-12	9.3e-04	-9.854826e-01	0.6	
24	0.940	0.964	3.0e-09	1.6e-12	5.4e-05	-9.855364e-01	0.6	
25	1.000	0.899	1.8e-08	4.6e-12	1.6e-05	-9.855383e-01	0.6	
26	1.000	1.000	1.0e-08	3.0e-12	6.9e-07	-9.855386e-01	0.6	
27	1.000	1.000	1.1e-08	3.4e-12	1.5e-08	-9.855386e-01	0.7	

Stop: max(relative gap, infeasibilities) < 1.00e-07

number of iterations	= 27
primal objective value	= -9.85553456e-01
dual objective value	= -9.85523662e-01
actual relative gap	= -1.50e-05
gap := trace(XZ)	= 1.51e-08
relative gap	= 1.51e-08
primal infeasibilities	= 1.06e-08
dual infeasibilities	= 3.41e-12
Total CPU time (secs)	= 0.8
CPU time per iteration	= 0.0
termination code	= 0

info: 'No problems detected (SDPT3)'

```

> gamma minimal: 0.98552
> M=[-0.6285 -4.8167e+03]           DF=[0 0]
+ Processing Ptilde
+ Processing myklmi => rank(I-RS)< n => dim(Aaug):6 - dim(AF):5
+ Processing postanalyse
Performance Hinf obtenue: De klmi: 0.98552 - De norminf: 0.98786

```

All numerical indicators are green !

The μ_g analysis procedure

- The procedure involves sufficient conditions ($H_- \rightarrow H_\infty$, small gain theorem)
 - The nature (i.e. real and/or complex) and the structure (block diagonal) of Δ is not taken into account.

$\Rightarrow \gamma < 1 \rightarrow$ what about the conservativeness ?

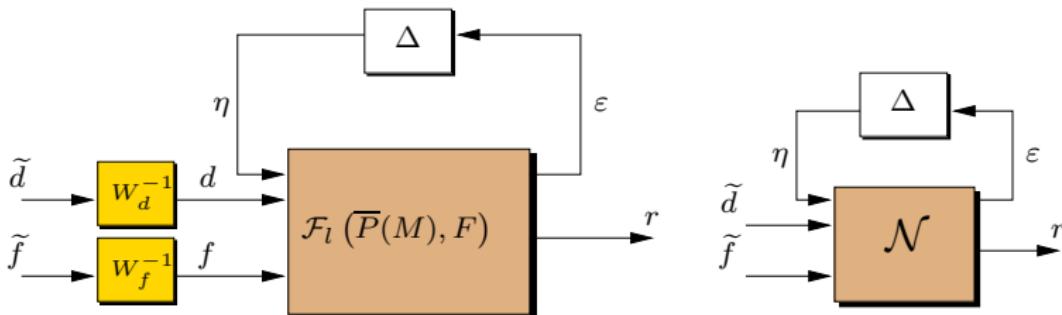
$\Rightarrow \gamma \geq 1 \rightarrow F(s), M_y, M_u = \text{May be an admissible solution !}$

Post-analysis of robust fault detection performance

⇒ the generalized structured singular value μ_g (Newlin and Smith, 1998; Henry 2002; Henry, 2005; Henry, 2006; Falcoz et al. 2010)

The μ_g analysis procedure

Consider W_d and W_f . With some LFR manipulations



Problem formulation

With the computed solution $M_y, M_u, F(s)$:

$$||T_{r\tilde{d}}||_\infty < 1 \text{ and } ||T_{r\tilde{f}}||_- > 1 \quad \forall \Delta \in \underline{\Delta} : ||\Delta||_\infty \leq 1$$

or (which is strictly equivalent)

$$\sup_{\omega} \overline{\sigma}(T_{r\tilde{d}}(j\omega)) < 1 \text{ and } \inf_{\omega \in \Omega} \underline{\sigma}(T_{r\tilde{f}}(j\omega)) > 1 \quad \forall \Delta \in \Delta : \|\Delta\|_\infty \leq 1$$

The μ_g analysis procedure

Theorem (Henry, 2005)

Let $\mathcal{N} = \begin{pmatrix} \mathcal{N}_{11} & \mathcal{N}_{12} \\ \mathcal{N}_{21} & \mathcal{N}_{22} \end{pmatrix}$ so that $\mathcal{N}_{22} = T_{r\tilde{f}}|_{\Delta=0}$. Assume that

$$\sup_{\omega} \mu_{\underline{\Delta}}(\mathcal{N}_{11}(j\omega)) < 1$$

where $\overline{\Delta} = \{diag(\Delta, \Delta_d)\}$. $\Delta_d \in \mathbb{C}^{q_{\tilde{d}} \times q_r}$. Assume that $\mathcal{N} \in \text{dom}(\mu_g)$. Then **a necessary and sufficient condition** for $(M_y, M_u, F(s))$ to satisfy the requirements W_d/W_f is:

$$\boxed{\sup_{\omega \in \Omega} \mu_{g\widehat{\Delta}}(\mathcal{N}(j\omega)) < 1}$$

$\widehat{\Delta} = \{\text{diag}(\overline{\Delta}, \Delta_f)\}$. $\overline{\Delta}$ is the structure associated to $\underline{\Delta}$ and $\Delta_f \in \mathbb{C}^{q_{\tilde{f}} \times q_r}$.

Applications:

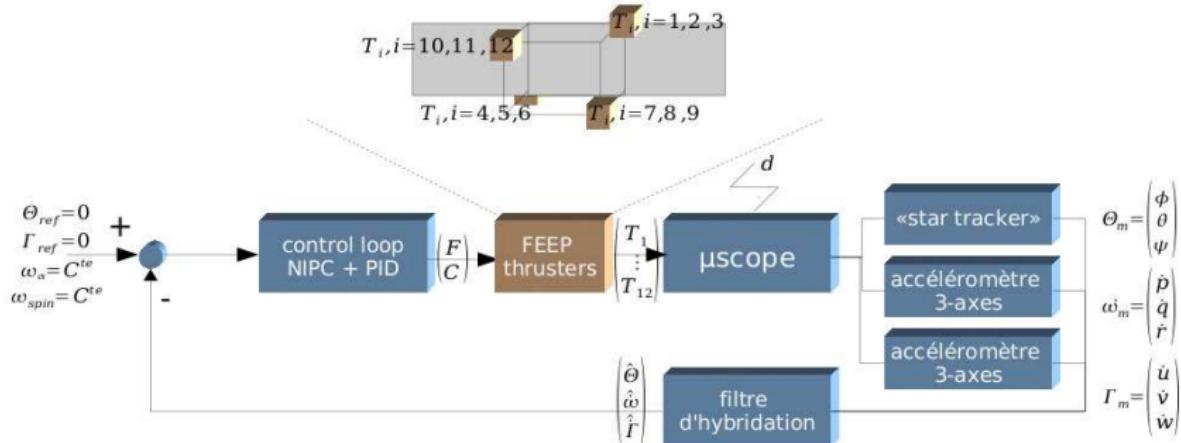
- ① The *Microscope* satellite - CNES / IMS (Henry,2008)
 - ② The *HL20* Reentry Vehicle - ESA / Astrium ST / IMS (Falcoz et al., 2008 - 2010)
 - ③ The *MSR* Rendez-vous mission - Thales Alenia Space / IMS

Microscope

- Scheduled to be launched in 2011
- Mission: test the validity of the equivalence principle (Einstein, 1911) using space-based measurements with a precision higher than 10^{-13} .
- Orbit: circular, quasi polar, sun synchronous - Alt: 700km
- Disturbances
 - Photonic pressure: solar / albedo terrestrial
 - Earth magnetic field
 - Earth gravitational field
 - High atmospheric winds
 - Measurement noises (non perfect NAV module)
- Fault to be detected
 - Actuator (ionic thrusters) faults



Microscope



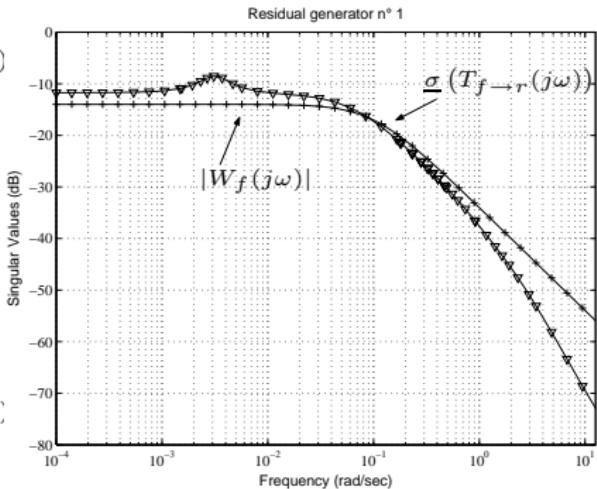
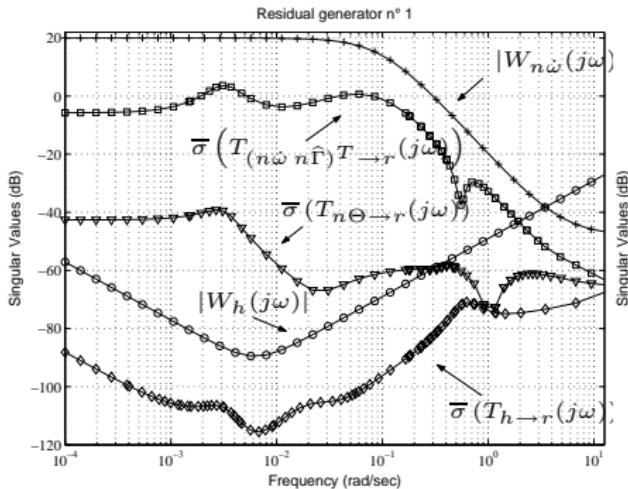
Taking into account the AOCS actions (PID + allocation module) + actuator models + satellite dynamics (small angles assumption) + NAV (Pade approximation + former filters) + additive faults model

$$y = P \begin{pmatrix} d \\ f \\ u \end{pmatrix}, \quad u = Ky \quad (\text{i.e. } \Delta = 0)$$

12 H_∞/H_- filters
(DOS strategy)

Microscope

- The shaping filters (and the principal gains of the transfers)

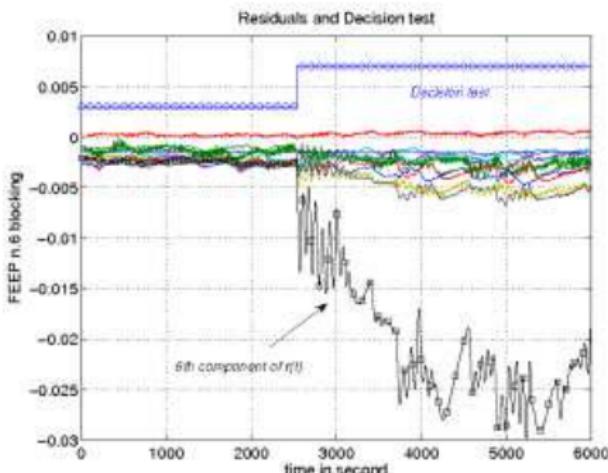
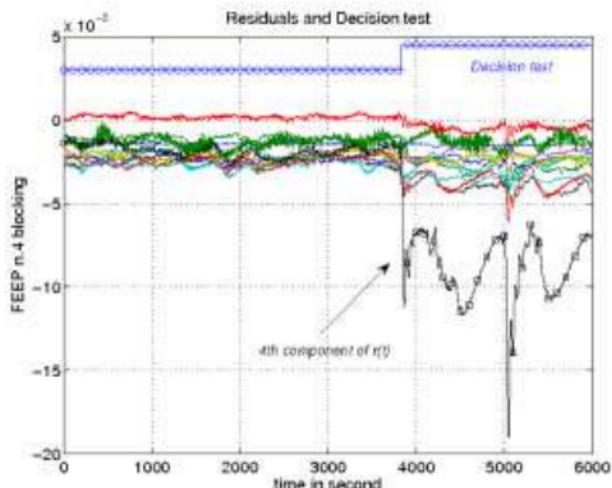


Robustness requirements (left) and Fault sensitivity objectives (right)

- $W_h \rightarrow$ centered around ω_{spin}
 - $W_n \rightarrow$ Star Tracker (constant) - Accelerometers (high frq)
 - $W_f \rightarrow$ Low frequency requirements $\omega \in]0; 0.1] \text{rd/s}$

Microscope

- Nonlinear simulations



Thruster n.4 closed (left) - thruster n.6 jammed (right)

The HL-20 RLV

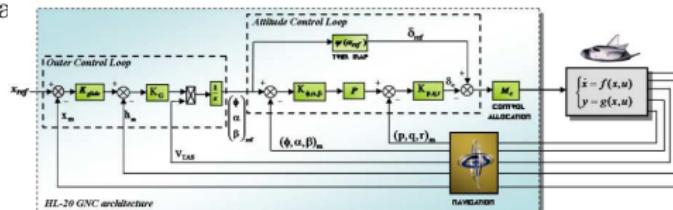
- Flight trajectory: TAEM (mach 2.5 → mach 0.5) + Auto-landing (mach 0.5 → runway)

- Model perturbations:
CoG, mass, inertia, aeros., coeff

- Disturbances:
 - Winds and Atmospheric disturbances
 - Non perfect NAV
 - Faults to be diagnosed: Left/Right flaps

- Modeling the GNC
 - gain-scheduling control laws
 - dynamic pressure dependent allocation module

- The HL-20 dynamics
 - trim analysis (fault free / faulty situations)
 - linear approximation around the flight trajectory

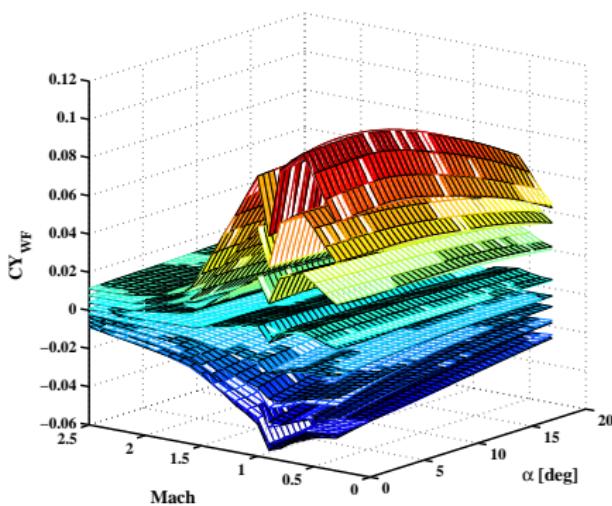
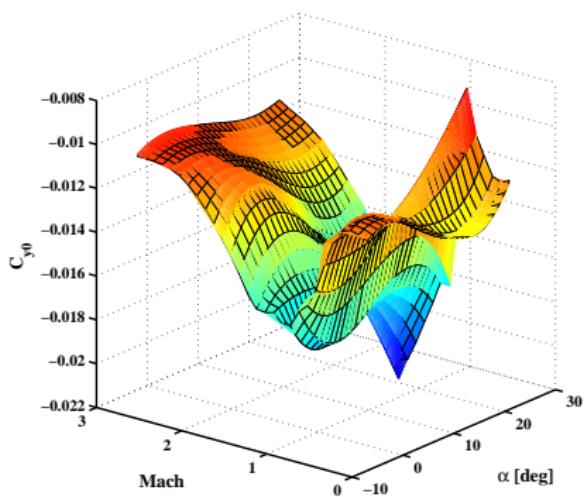


2 H_∞/H_- filters (DOS strategy)

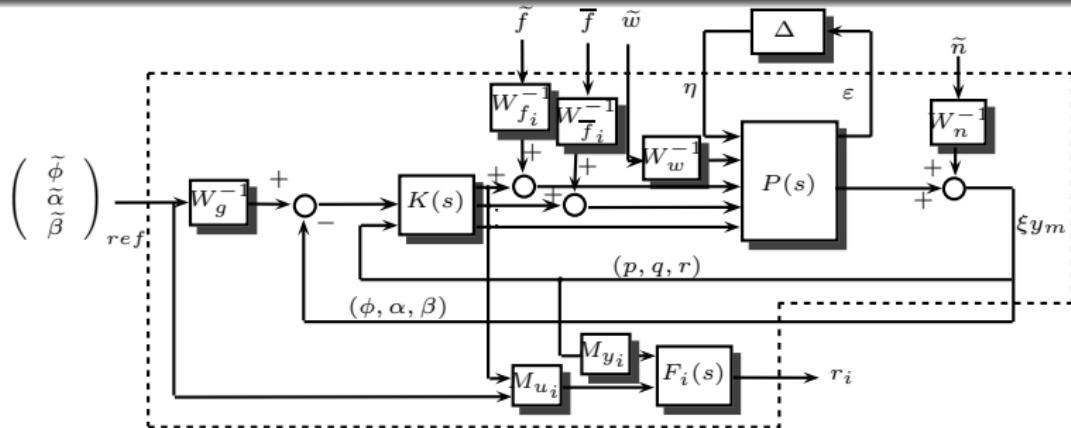
The HL-20 RLV

Modeling the aerodynamic coefficients:

- Polynomial interpolation (1D) + PCA (2D): auto-landing phase
 → \mathcal{C}^∞ neural network-based models: TAEM phase



$C_{y0}(\alpha, mach)$ (lateral lift) and $C_{Y_{wfl}}(\alpha, \beta, mach)$ (left wing flap)



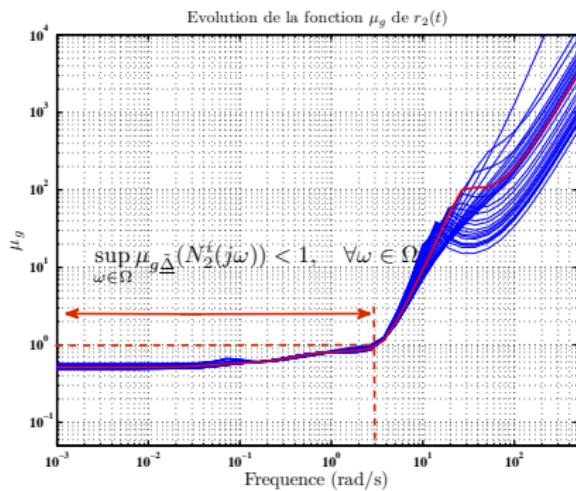
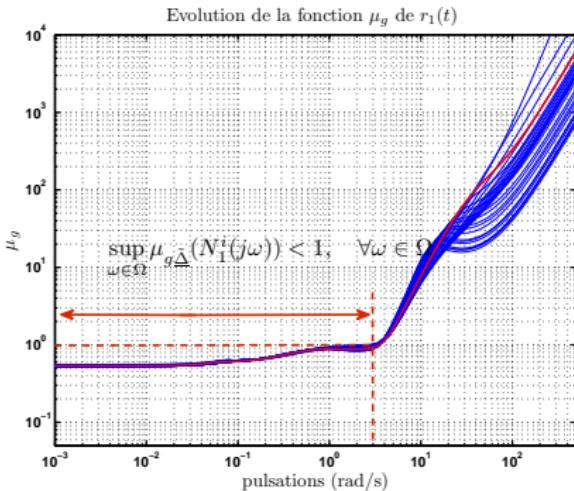
$$\Delta = \text{diag}\{\delta_{C_{l0}}, \delta_{C_{m0}}, \delta_{C_{n0}}, \delta_{C_{x0}}, \delta_{C_{y0}} I_3, \delta_{C_{z0}} I_3, \delta_{X_{cg}} I_2, \delta_{I_{xx}} I_2, \delta_{I_{yy}} I_3, \delta_{I_{zz}} I_3, \delta_m I_3\}$$

$$\Rightarrow \Delta \in \mathbb{R}, |\delta_i| \leq 1$$

- Atmospheric disturbances (Dryden filters): $W_{wu} = \gamma_w (\sigma_{ug} \sqrt{\frac{L_{ug}}{\pi V}} \frac{1+\tau s}{1+\frac{L_{ug}}{V_{TAS}} s})^{-1}$
 - Guidance signals: $W_g = \gamma_g I_3$
 - Navigation module: $W_n = \gamma_n \frac{1+\frac{1}{250}s}{1+\frac{1}{100}s} I_{10}$
 - Fault sensitivity objectives: $W_{f_i} = \gamma_{f_i} \frac{1}{1+\tau_{f_i}s}, \quad \tau_{f_i} = \frac{1}{\omega_{f_i}}, \quad \omega_{f_i} = 3rd/s, \quad i = 1, 2$

The HL-20 RLV

- The μ_g -analysis (V_{ref} parametrization)

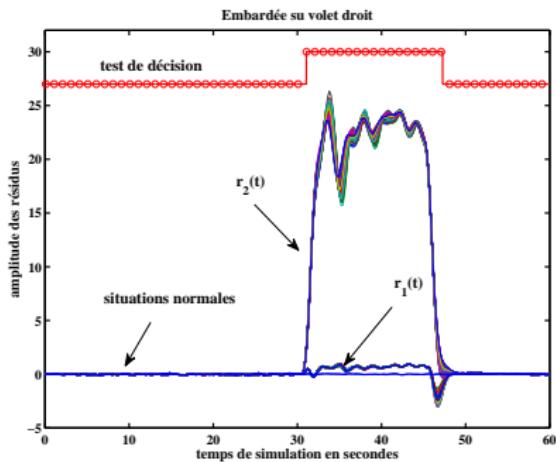
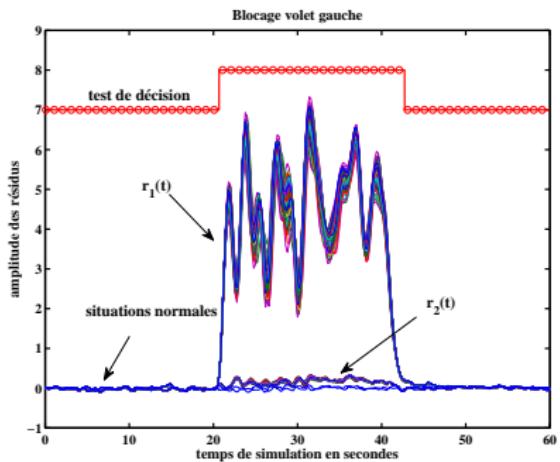


$$\sup_{\omega \in \Omega} \mu_{g_{\Delta}^{\widehat{\Delta}}}(\mathcal{N}_i(j\omega)) < 1, \quad i = 1, 2, \quad \Omega = [0; 3rd/s]$$

All required robustness/fault sensitivity specifications are met $\forall \Delta$, all along the reentry flight trajectory.

The HL-20 RLV

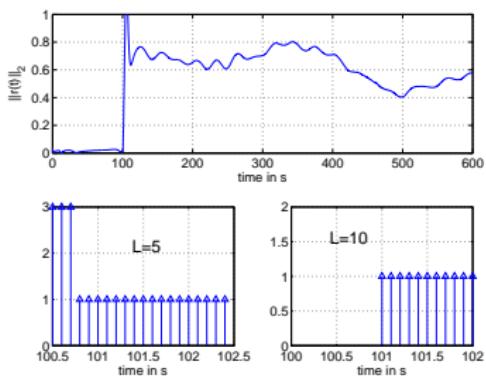
- Nonlinear simulations (Monte-Carlo campaign)



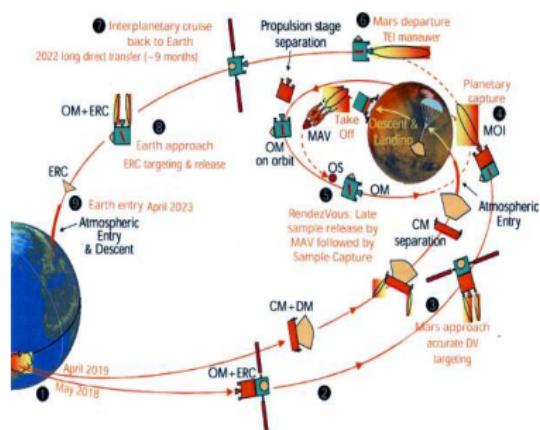
Left wing flap jammed (left) - right wing flap runaway (right)

The MSR rendez-vous mission

- Mission: Return tangible samples from Mars atmosphere/ground.
 - Five spacecrafts: an Earth/Mars transfer vehicle, an orbiter, a descent module, an ascent module and an Earth re-entry vehicle ⇒ **Focus on the RDV phase**
 - Fault to be detected: Thruster faults
 - FDI scheme:
 - A $H(0)$ observer + $\lambda_i \{A - LC\} < \Lambda_i$
 - Cross-correlation test:
$$\min_i \text{corr}\{r_j(t), u_{thr,i}(t + \tau)\} \quad i = 1 \dots 8$$



Fault in thruster 1



Concluding remarks: Extension to LPV problems

LPV formalism = an efficient paradigm to model nonlinear systems

- qLPV formulation (Biannic,1996; Leith,2000; Bruzelius,2004; Marcos,2005...)

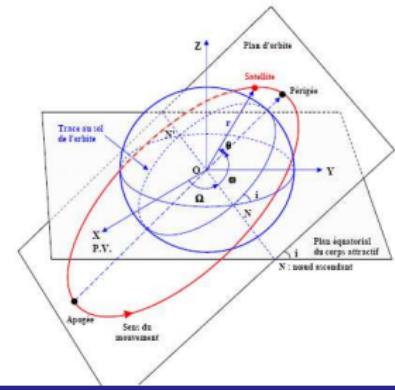
$$\begin{cases} \dot{x}_1 = -x_2 \\ \dot{x}_2 = x_1 + \alpha(1 - x_1^2)x_2 \end{cases} \stackrel{\theta=x_1}{\Rightarrow} \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} 0 & -1 \\ 1 & \alpha(1 - \theta^2) \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$$

- First order approximation around a reference trajectory
 \Rightarrow an adequate formalism for aerospace missions
 \Rightarrow known trajectory (x_0, u_0)

$$\left\{ \begin{array}{l} \dot{x} = f(x, u) \\ y = g(x, u) \end{array} \right. \xrightarrow{\theta = [x_0^T \ u_0^T]^T} \left\{ \begin{array}{l} \delta \dot{x} = A(\theta) \delta x + B(\theta) \delta u \\ \delta y = C(\theta) \delta x + D(\theta) \delta u \end{array} \right.$$

$$A(\theta) = \nabla_x f(x_0, u_0), \quad B(\theta) = \nabla_u f(x_0, u_0)$$

$$C(\theta) = \nabla_x g(x_0, u_0), \quad D(\theta) = \nabla_u g(x_0, u_0)$$



Concluding remarks: Extension to LPV problems

- A framework to model gain-scheduling controllers, NDI-based control laws... (Papageorgiou, 2005; Falcoz, 2007; Bokor, 2010)

Concluding remarks: Extension to LPV problems

- A framework to model gain-scheduling controllers, NDI-based control laws... (Papageorgiou, 2005; Falcoz, 2007; Bokor, 2010)

Performance measures: An induced I/O signal-based definition

$$\|T_{rd}(\theta)\|_\infty = \sup_{\substack{\forall \theta \\ \|d\|_2 \neq 0}} \frac{\|r\|_2}{\|d\|_2} \quad \|T_{rf}(\theta)\|_- = \inf_{\substack{\forall \theta \\ \|f\|_e \neq 0}} \frac{\|r\|_e}{\|f\|_e}, \dim(r) = 1$$

robustness

fault sensitivity

(Grenaille & Henry, 2008; Henry, 2009)

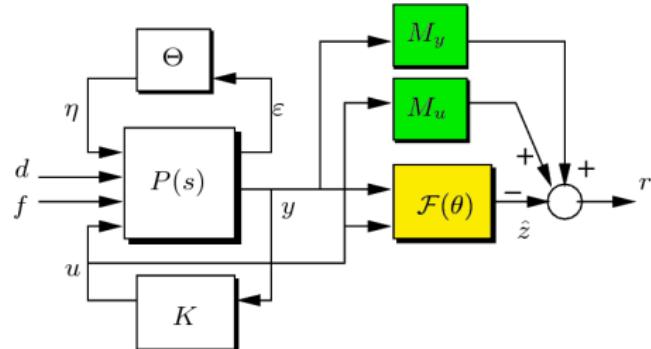
Concluding remarks: Extension to LPV problems

Assumptions: $\theta_i(t)$ are measured in real time and bounded ,i.e. $|\theta_i(t)| \leq 1 \forall t$

$$y = F_u(P, \Theta) \begin{pmatrix} d \\ f_i \\ u \end{pmatrix}, \quad d = \begin{pmatrix} w^T & v^T & \bar{f}_i^T \end{pmatrix}^T$$

$\Theta = blockdiag \left(\theta_1 I_{k_1}, \dots, \theta_q I_{k_q} \right)$ so that

$$\Theta \subset \mathbb{R}, \quad ||\Theta||_\infty \leq 1$$



Problem:

Derive M_y , M_u and the (stable) LPV filter $\mathcal{F}(\theta) = F_l(F, \Theta)$ so that

$F(s) = \begin{pmatrix} C_{F1} \\ C_{F\theta} \end{pmatrix} (sI - A_F)^{-1} \begin{pmatrix} B_{F1} & B_{F\theta} \end{pmatrix} + \begin{pmatrix} D_{F11} & D_{F1\theta} \\ D_{F\theta 1} & D_{F\theta\theta} \end{pmatrix}$ that solve the following optimization problem

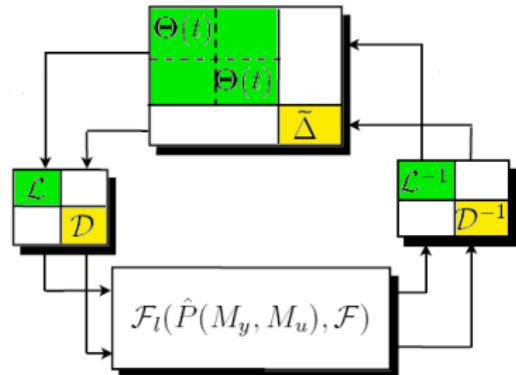
$$\min_{M_y, M_u, F} \quad \gamma_1 \\ s.t. \quad \|T_{d \rightarrow r}(\theta)\|_\infty < \gamma_1$$

$$\begin{array}{ll} \max_{M_y, M_u, F} & \gamma_2 \\ \text{s.t.} & \|T_{f \rightarrow r}(\theta)\|_{sens} > \gamma_2 \end{array}$$

- Solution: the scaling matrices technique (Henry,2009)

Let L_{Δ} and $L_{\mathcal{D}}$ be the sets of matrices:

$$\begin{aligned} L_\Delta &= \{L > 0 : L\Theta = \Theta L, \forall \Theta \in \Delta\} \\ \Rightarrow L_{\Delta \oplus \Delta} &= \{\mathcal{L}diag(\Theta, \Theta) = diag(\Theta, \Theta)\mathcal{L}\} \\ L_{\mathcal{D}} &= \left\{ \mathcal{D} > 0 : \mathcal{D}\tilde{\Delta} = \tilde{\Delta}\mathcal{D}, \forall \tilde{\Delta} \right\} \end{aligned}$$



The scaled H_∞ problem

$\mathcal{F}(\theta)$ is internally stable $\forall \theta(t)$ and there exists a solution to the problem if $\exists \gamma < 1, M_u, M_u$ and $F(s)$:

$$\left\| \begin{pmatrix} \mathcal{L}^{1/2} & 0 \\ 0 & \frac{1}{\sqrt{\gamma}}\mathcal{D} \end{pmatrix} F_l \left(\tilde{P}(M_y, M_u), F \right) \begin{pmatrix} \mathcal{L}^{-1/2} & 0 \\ 0 & \frac{1}{\sqrt{\gamma}}\mathcal{D}^{-1} \end{pmatrix} \right\|_{\infty} < 1$$

Pictures from space: ATV de-docking

- ① Docking: 3rd April 2008
 - ② De-docking: 5th September 2008

Thank you for listening